



**NPIC** 中国核动力研究设计院  
NUCLEAR POWER INSTITUTE OF CHINA



# The microstructure of post-irradiated A508-3 steel and its effects on Charpy impact energy

Lu Wu, Wei Zhang, Shaoyu Qiu, Xiaoyong Wu,  
Zhen Wang, Wen He, Bang Wen, Haisheng Zhang, Huajun Mo

<sup>1</sup> *The First Sub-institute, Nuclear Power Institute of China*

<sup>2</sup> *National Key Laboratory for Nuclear Fuel and Materials, Nuclear Power Institute of China*

18<sup>th</sup> September, Helsinki



# Contents



**Introduction**



**Experimental**



**Results and Discussion**



**Conclusions**



# Introduction



**Reactor Pressure Vessel**

## **Key issues :**

- Irradiation embrittlement

- ✓ One of the most important safety shield of the reactor
- ✓ Cannot change, determined the lifetime of the reactor

## **Severe conditions:**

- Neutron irradiation
- Multi-stress situation
- High temperature and thermal shock
- Water/steam corrosion
- .....



# Introduction

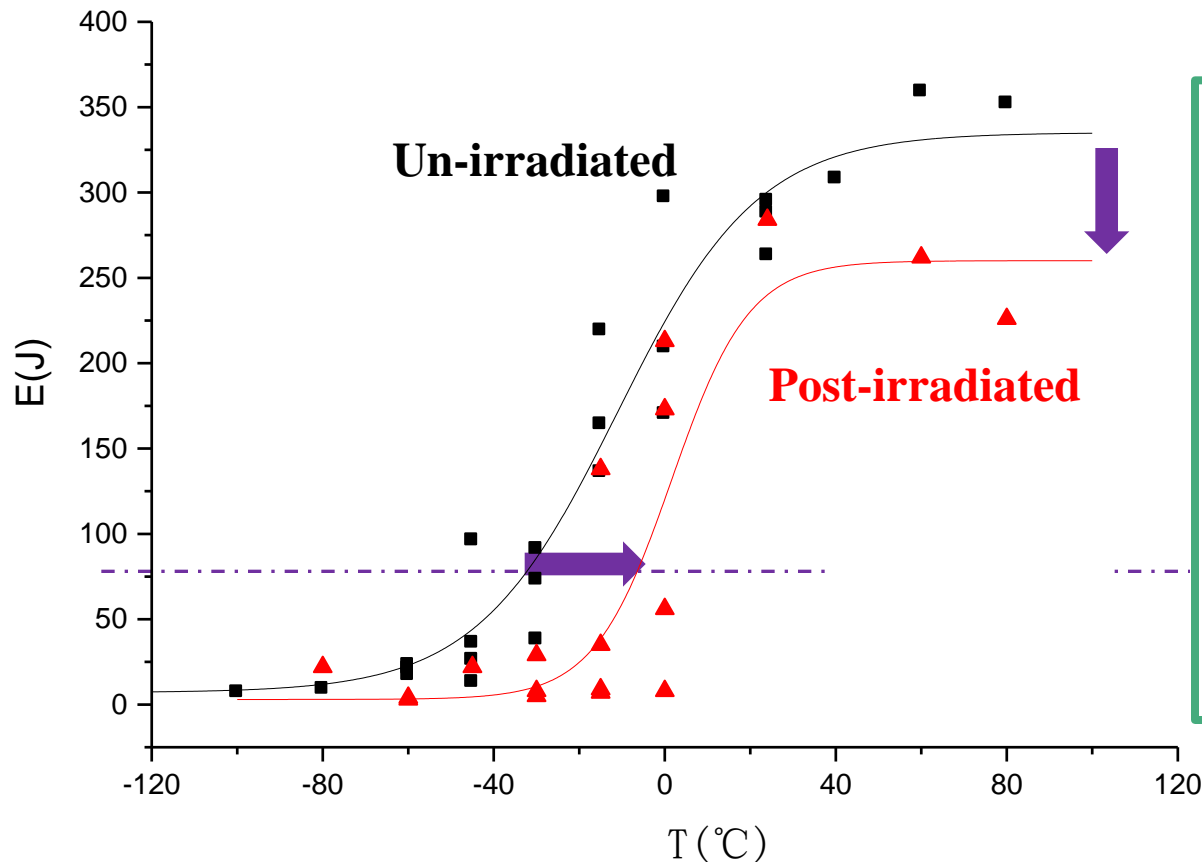
## The chemical compositions of LWR RPV steels (wt.%)

Materials	C	Si	Mn	S	<u>P</u>	Cr	Ni	<u>Cu</u>	Mo	V
American A508-III	≤0.2 5	0.15/0.4 0	1.20/1.5 0	≤0.02 0	≤0.02 0	<0.25	0.40/1.0	-	0.45/0.6 0	≤0.05
French 16MND5	≤0.2 0	0.10/0.3 0	1.15/1.5 5	≤0.00 8	≤0.00 8	<0.25	0.50/0.8 0	≤0.08	0.45/0.5 5	≤0.01
Japanese SQV2A	≤0.2 5	0.15/0.3 0	1.15/1.5 0	≤0.03 5	≤0.03 5	-	0.40/0.7 0	-	0.45/0.6 0	-
Russian 15×2HMΦ A1	0.13/ 0.18	0.17/0.3 7	0.30/0.6 0	≤0.01 2	≤0.01 0	1.8/2.3	1.0/1.5	≤0.08	0.5/0.7	0.10/ 0.12
Chinese A508-III	≤0.2 2	0.10/0.3 0	1.15/1.6 0	≤0.00 5	≤0.00 8	≤0.25	0.50/0.8 0	≤0.08	0.43/0.5 7	/





# Introduction



## Irradiation effects:

- Ductile-to-brittle transition temperature (DBTT) increase
- Maximum absorb energy decrease
- .....

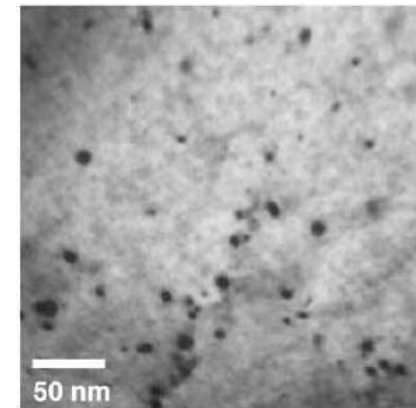
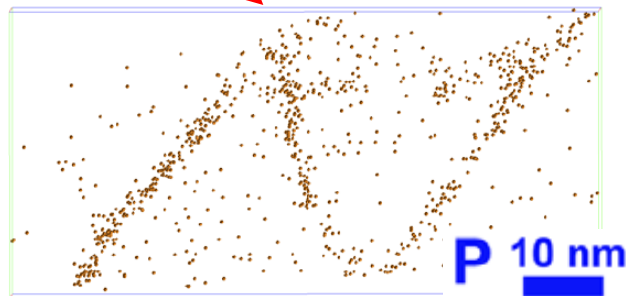
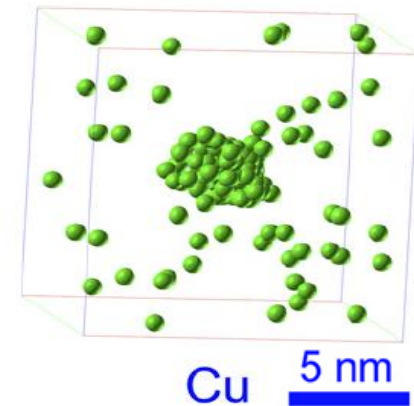
The Charpy V-notch impact energies of the A508-3 steel from the HFETR as a function of temperature for the un-irradiated and irradiated conditions at neutron fluence of  $2.97 \times 10^{19} \text{ n/cm}^2$



# Introduction

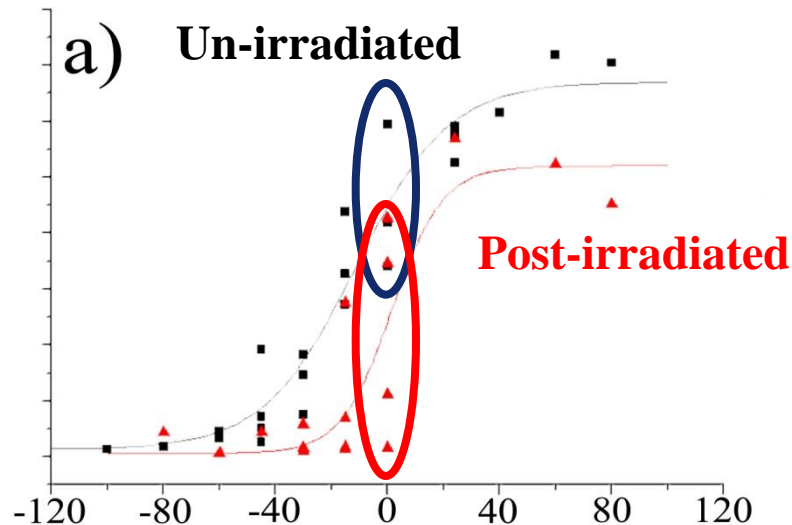
**The main reasons of the irradiation embrittlement of the RPV steel are:**

- The precipitation of nanoscale atomic clusters (Copper, Nickel, Manganese, etc.)
- The formation of dislocation loops inside matrix
- The segregation of Phosphorus atoms beyond boundary





# Introduction



Charpy V-notch impact energy curve of A508-3 steel

*Besides the irradiation embrittlement, the impact energies of un-irradiated and post-irradiated A508-3 steel under the same testing environment are unstable.*

**WHY?**

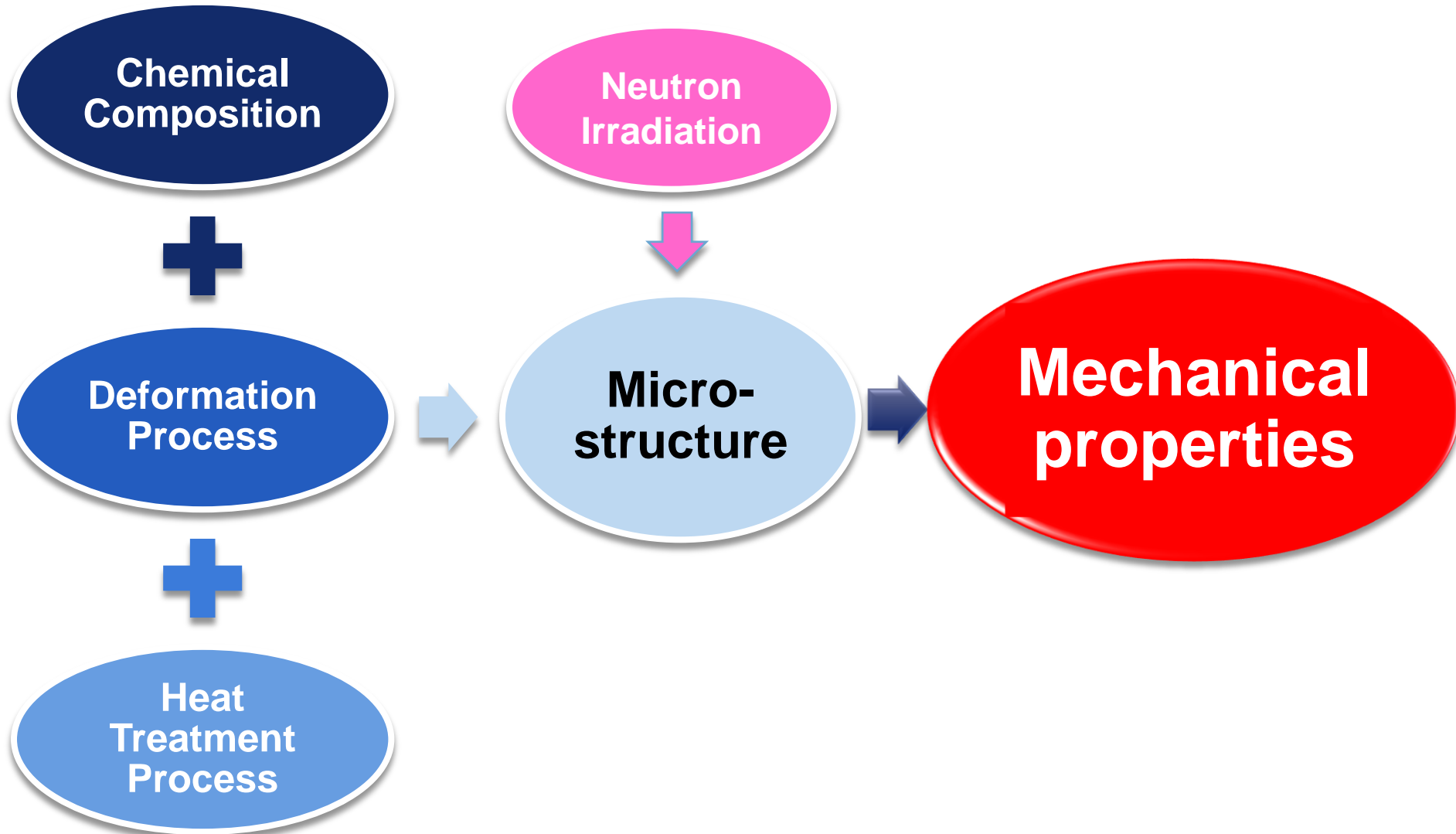
*Metallography?*

*Grain Size?*

*Defects?*



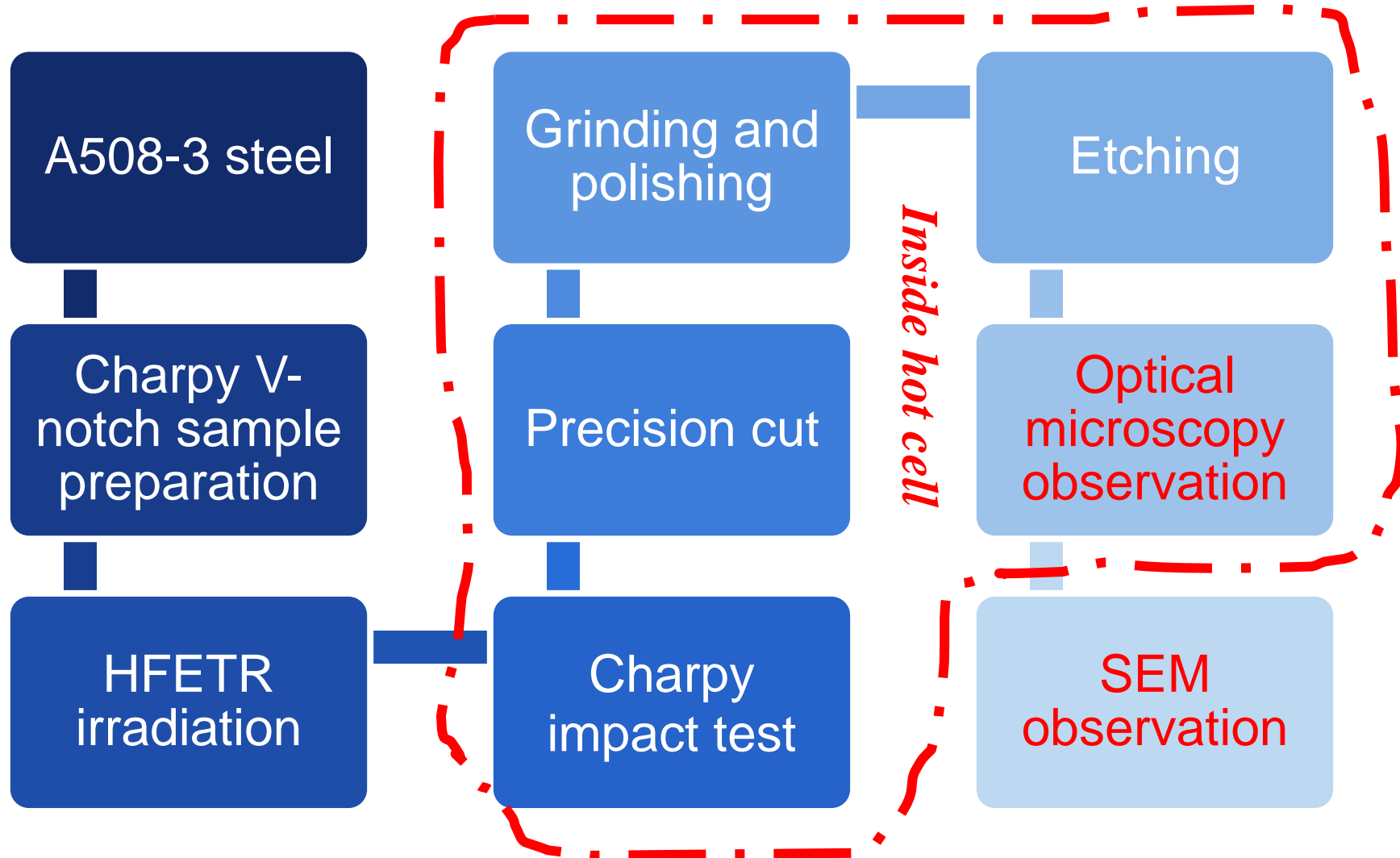
# Introduction







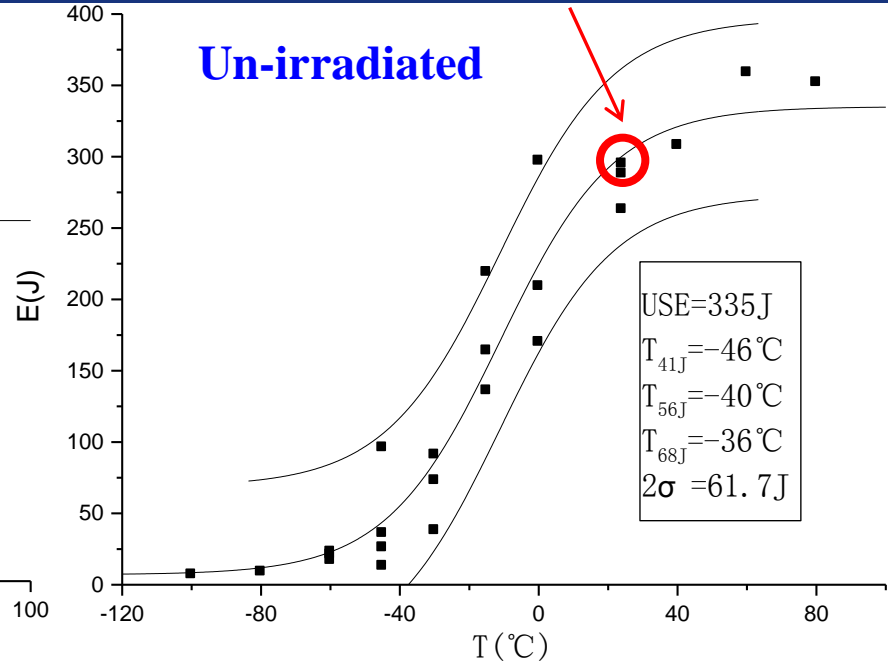
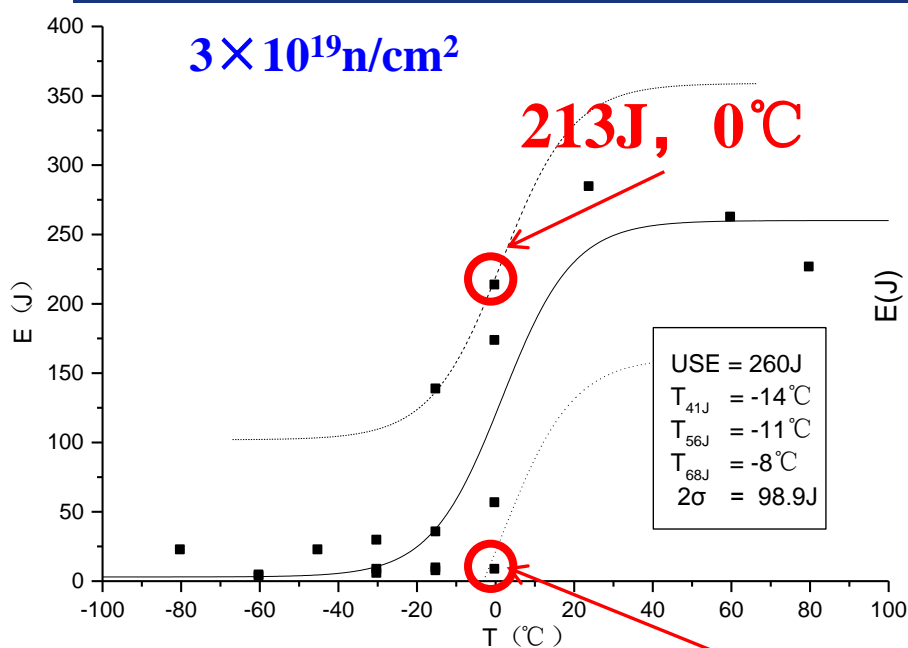
# Experimental





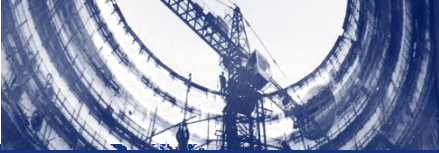
# Experimental

**263J, 24°C**

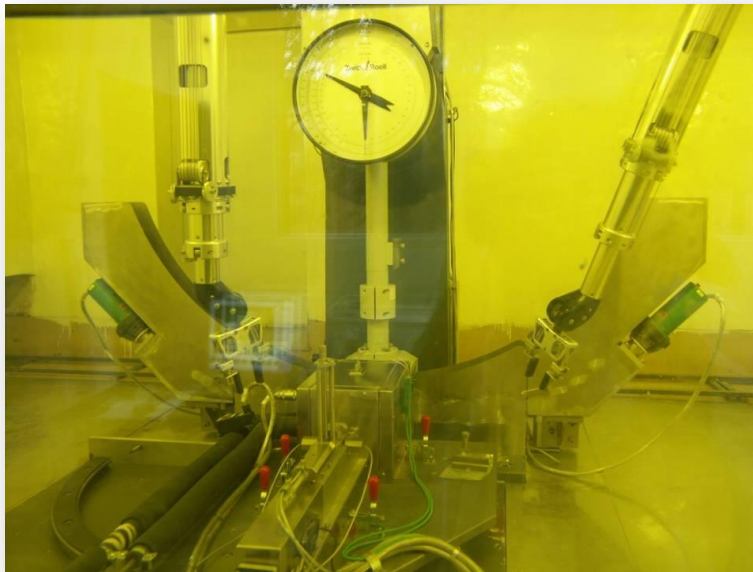


**Charpy V-notch impact energy curves of A508-3 steel**

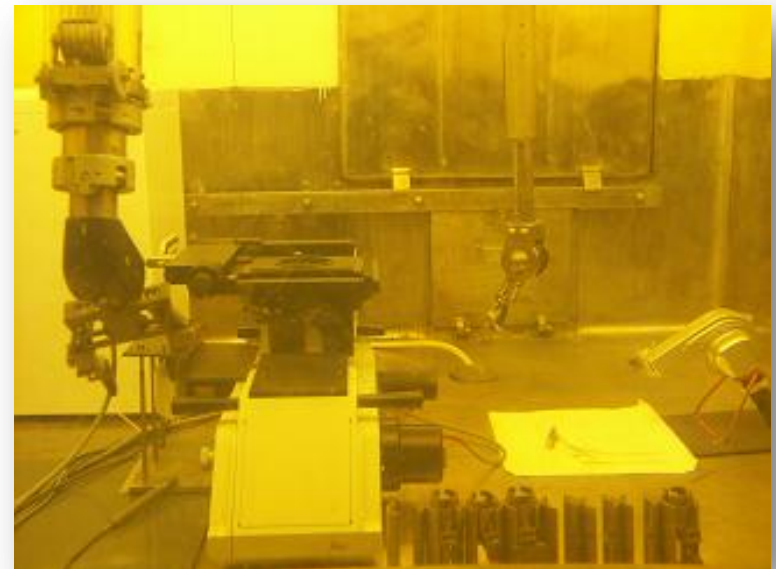
Samples	Irradiation Temperature	Neutron fluence ( $\text{n/cm}^2$ )	Test temperature	Charpy V-notch impact energy
	T ( $^\circ\text{C}$ )		T ( $^\circ\text{C}$ )	E (J)
1#	/	0	24	263
2#	$290 \pm 15$	$2.97 \times 10^{19}$	0	213
3#	$290 \pm 15$	$2.97 \times 10^{19}$	0	8



# Experimental



**Zwick RKP450 Charpy impact testing machine**



**Leica MEF4A Optical microscopy inside hot cell**



# Experimental



**FEI Quanta 450 FEG field emission scanning electron microscope with EDS  
inside a cast iron cell**



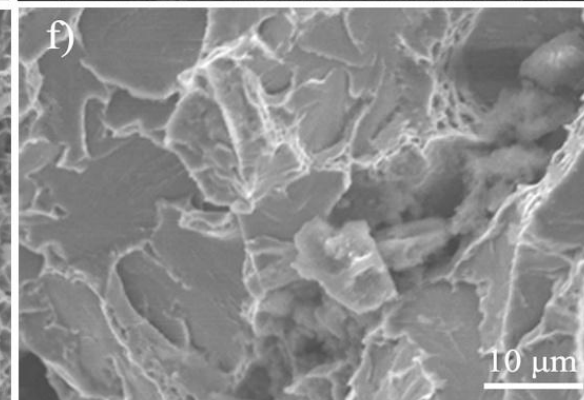
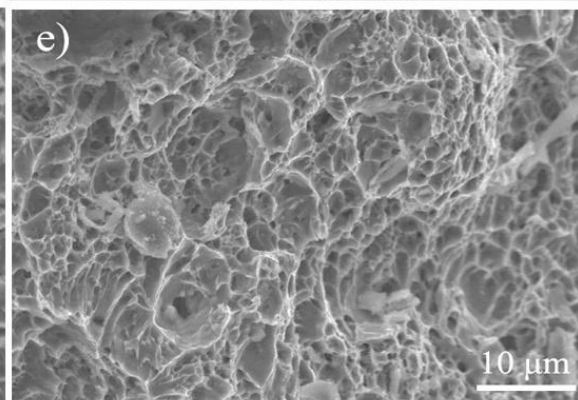
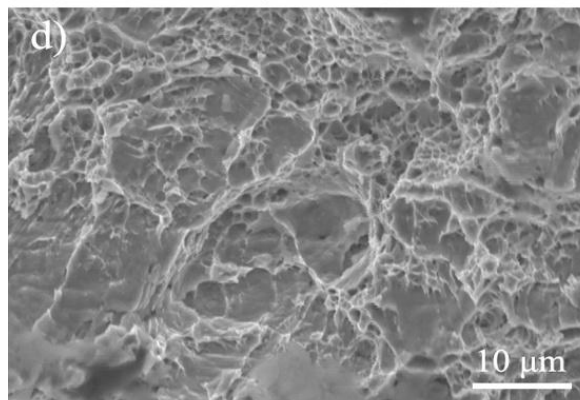
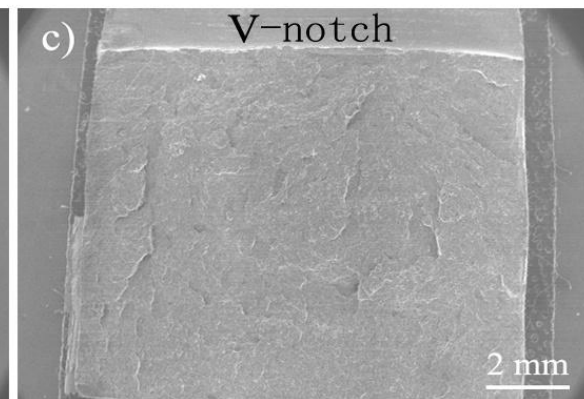
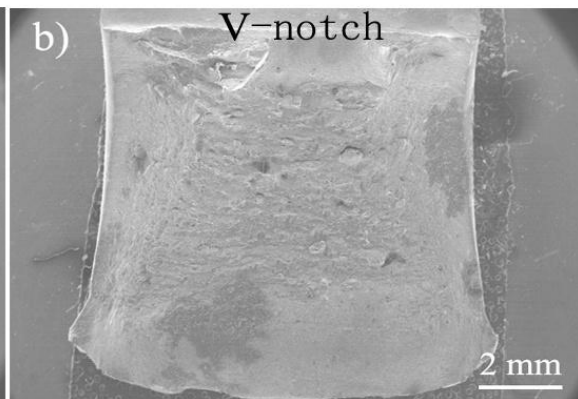
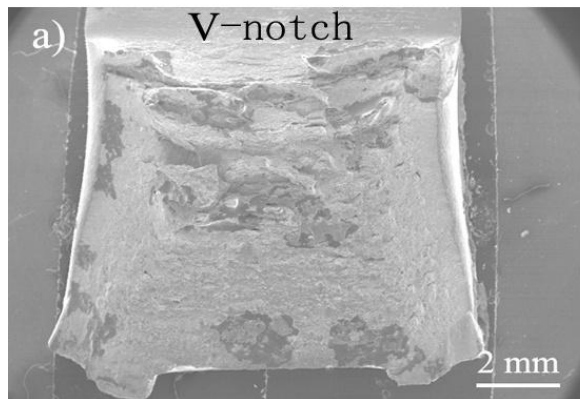


# Results and Discussion

**263J, 24°C**

**213J, 0°C**

**8J, 0°C**



**Unirradiated**

**$3 \times 10^{19} \text{ n/cm}^2$**

**$3 \times 10^{19} \text{ n/cm}^2$**

**SEM image of the fracture. Both for un-irradiated and post-irradiated samples, high impact energy means big deformation of the fracture(good impact toughness).**



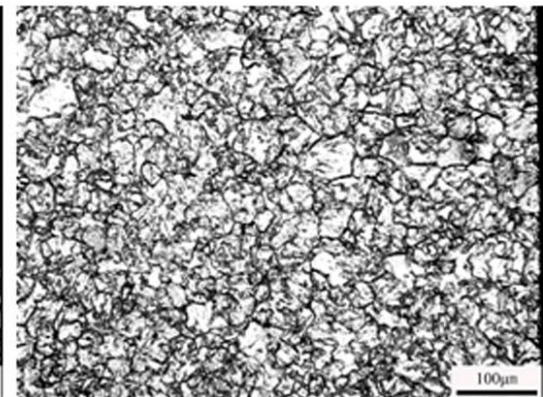
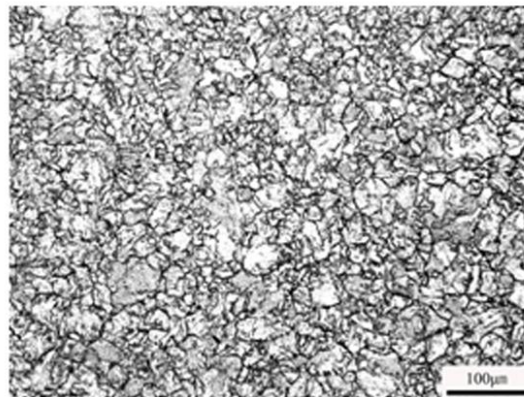
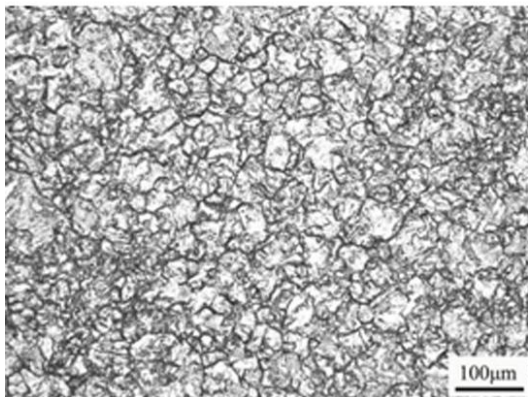
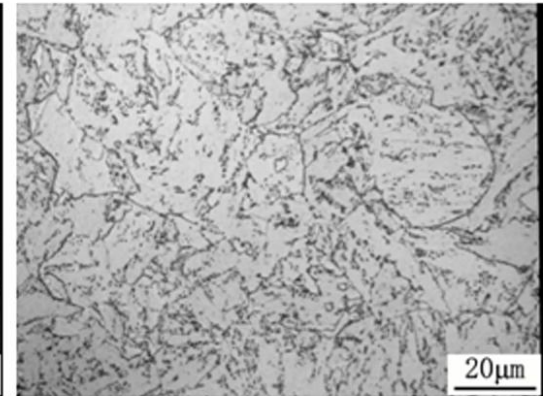
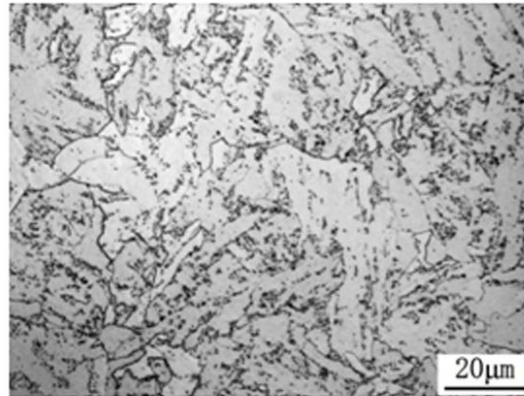
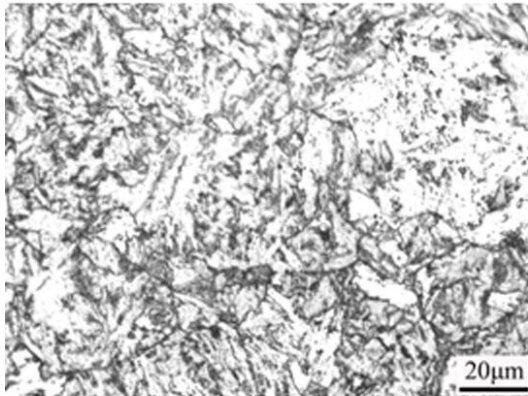


# Results and Discussion

263J, 24°C

213J, 0°C

8J, 0°C



Unirradiated

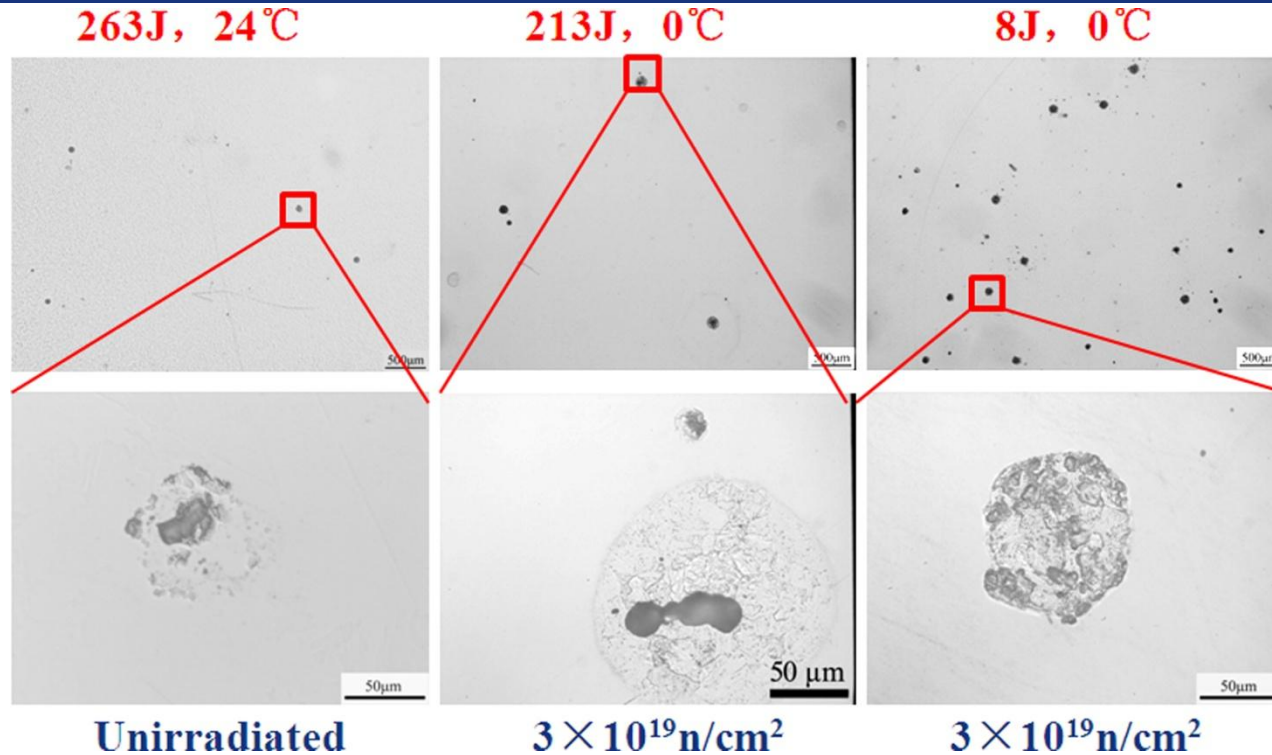
$3 \times 10^{19} \text{ n/cm}^2$

$3 \times 10^{19} \text{ n/cm}^2$

*Optical metallography(upper) and grain size(lower) images – No big differences between un-irradiated and post-irradiated samples*



# Results and Discussion



Unirradiated

$3 \times 10^{19} \text{ n/cm}^2$

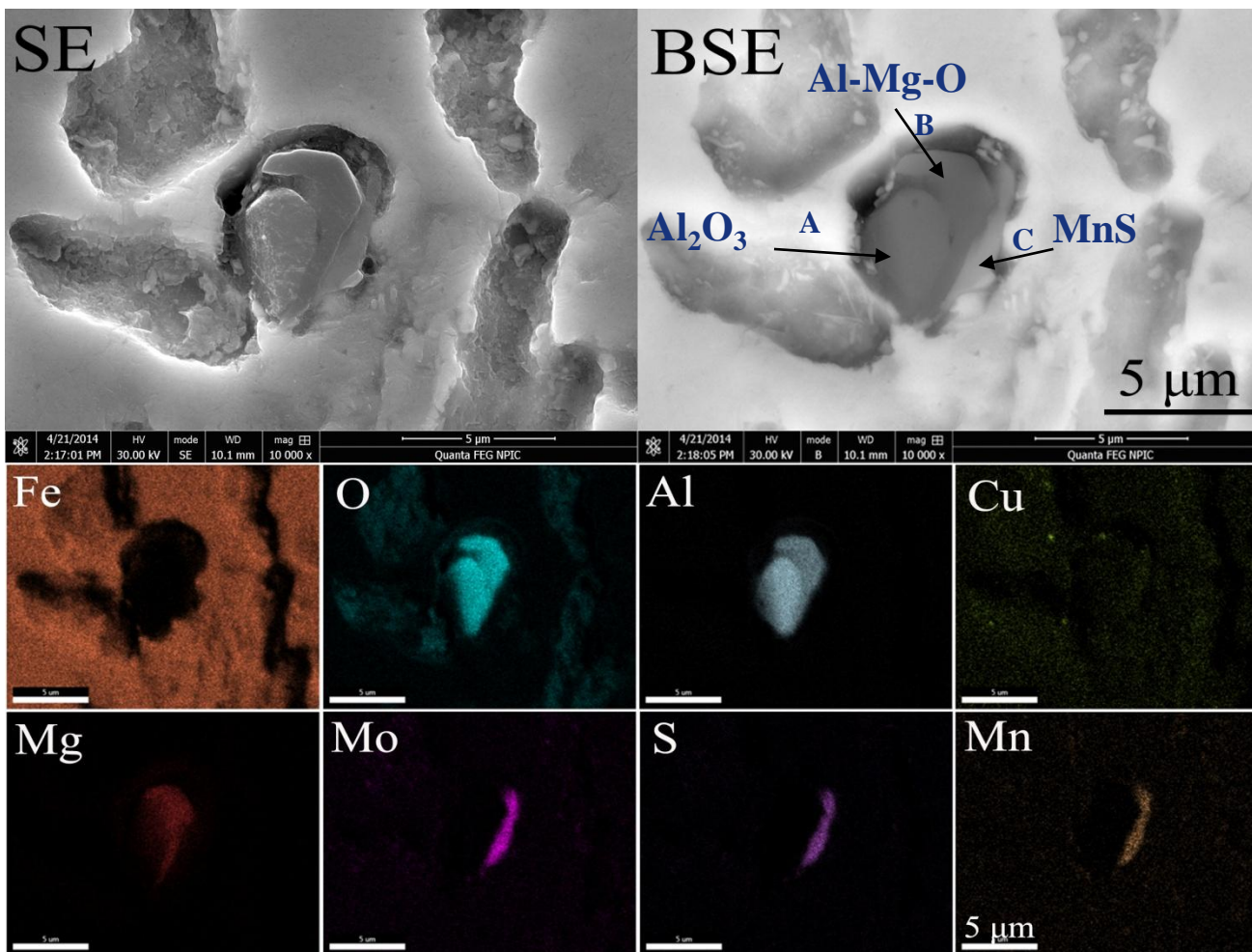
$3 \times 10^{19} \text{ n/cm}^2$

- ◆ *Observe after polishing directly(black points, defects). Optical images of morphology and distribution of defects/holes: Both for the un-irradiated and post-irradiated samples, the lower the absorb energy is, the higher the number densities of defects.*
- ◆ *The holes in not formed during irradiation, but probably formed during solidification process. Need further investigation.*





# Results and Discussion

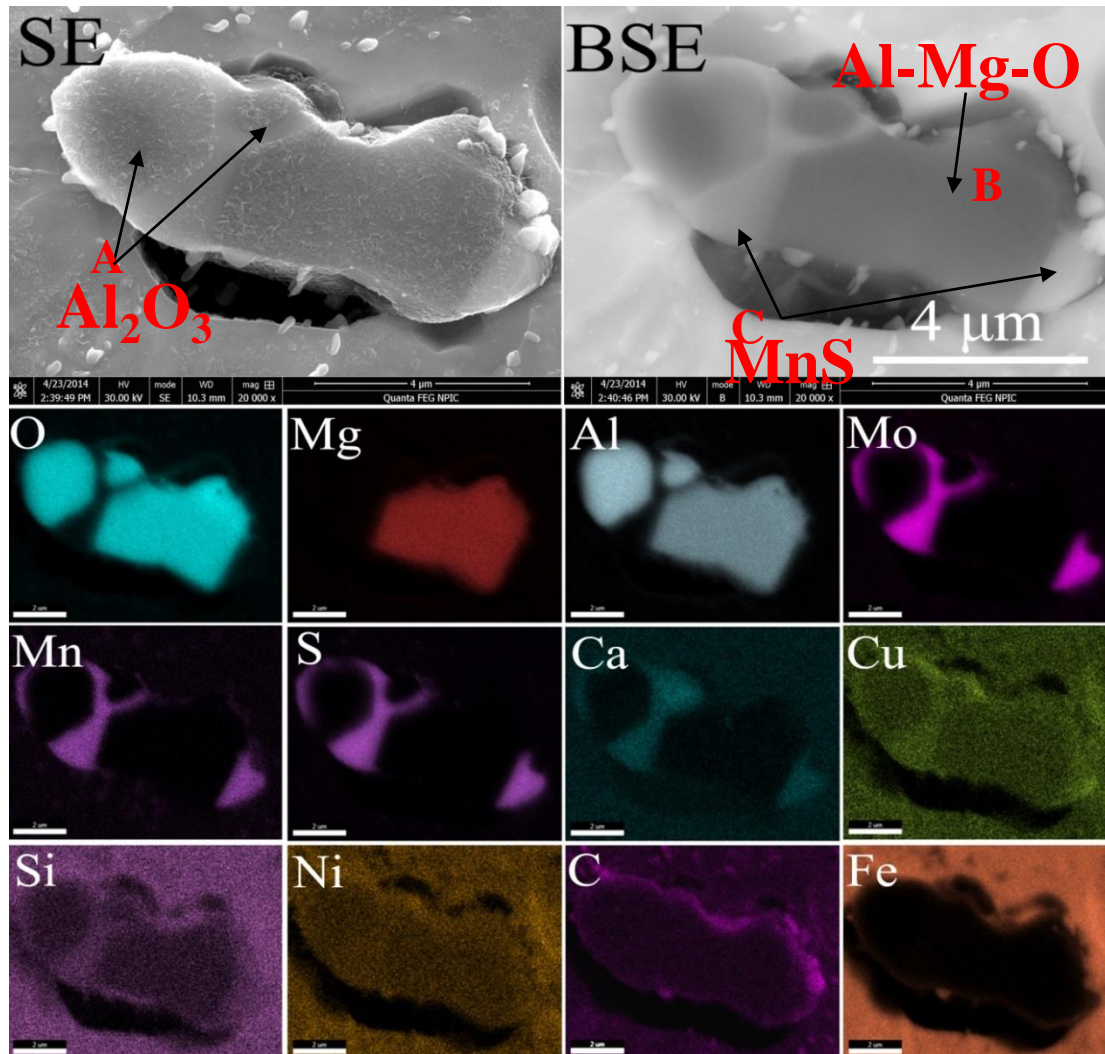


Positions	A	B	C
Fe	0.08	-	3.00
C	0.02	0.03	0.10
O	55.42	56.56	-
Al	44.34	29.89	0.27
Mg	-	13.52	-
Mo	-	-	1.38
S	-	-	44.20
Mn	-	-	42.74
Ca	-	-	6.49
Cr	-	-	0.25
Ni	-	-	0.37
Se	-	-	0.52
Cu	-	-	0.68
P	0.13	-	-
总计	100	100	100

1#, un-irradiated



# Results and Discussion



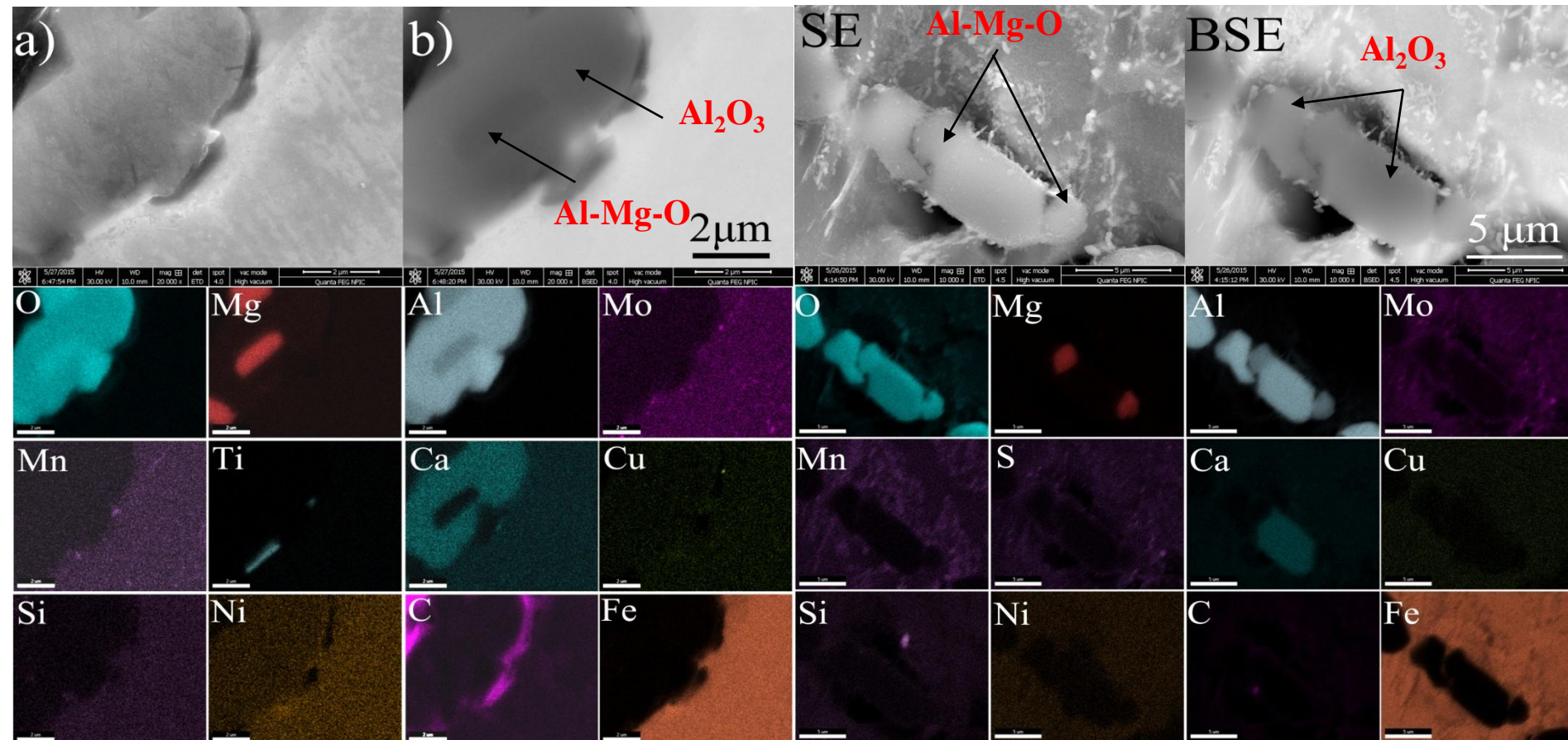
1#, un-irradiated

- ✓ The type of non-metallic inclusions can be easily distinguished by EDS. 3 kinds of non-metallic inclusions inside un-irradiated specimen:  $\text{Al}_2\text{O}_3$ ,  $\text{MnS}$ , and  $\text{Al-Mg-O}$  ternary phase ( $\text{MgAl}_2\text{O}_4$ , Spinel)
- ✓ The boundary between non-metallic inclusions and the matrix is quite loose





# Results and Discussion



2#, post-irradiated

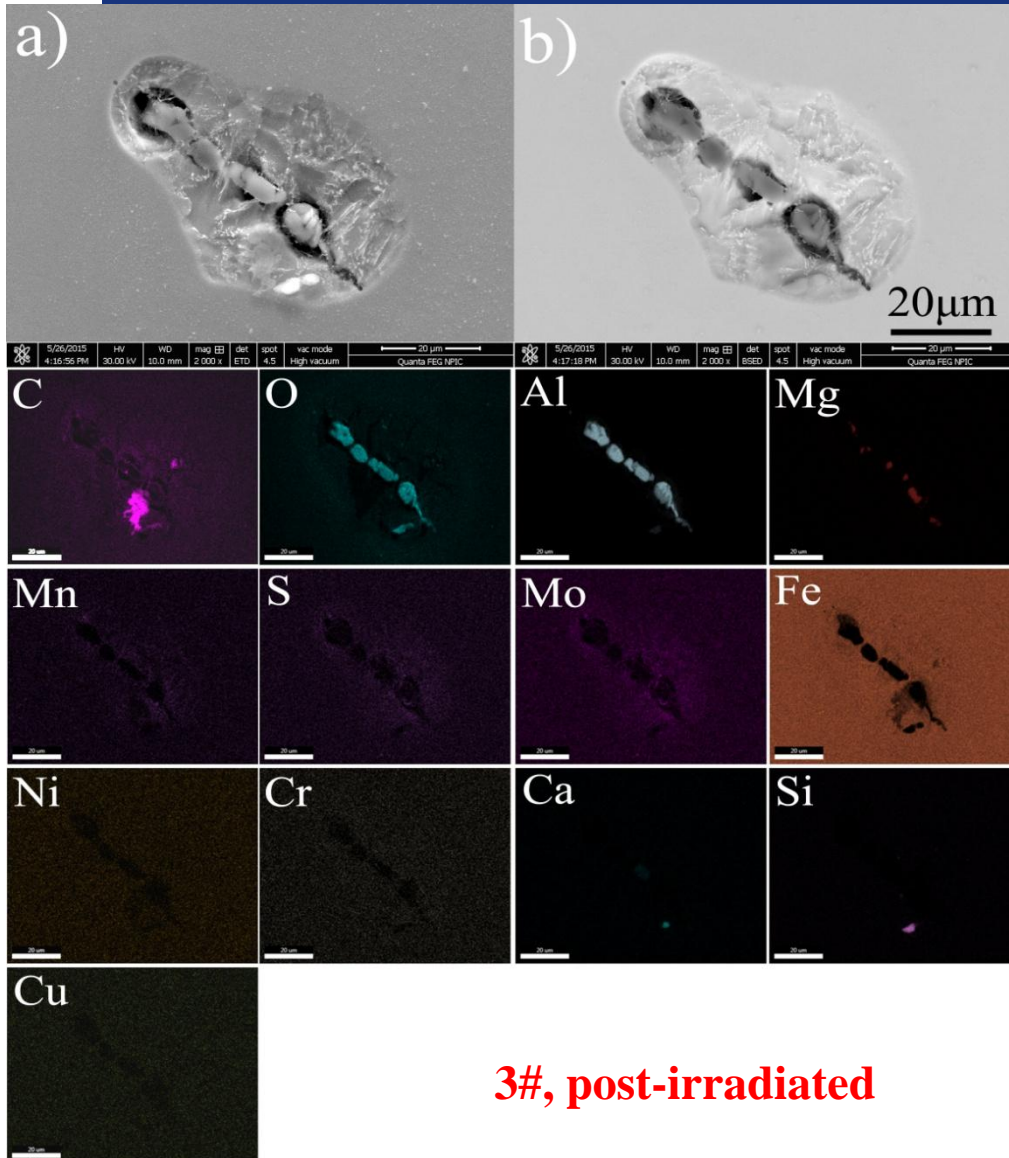
3#, post-irradiated

*Only 2 kinds of non-metallic inclusions existed in post-irradiated samples:  
 $\text{Al}_2\text{O}_3$  and  $\text{Al-Mg-O}$  ternary phase ( $\text{MgAl}_2\text{O}_4$ )*





# Results and Discussion



3#, post-irradiated

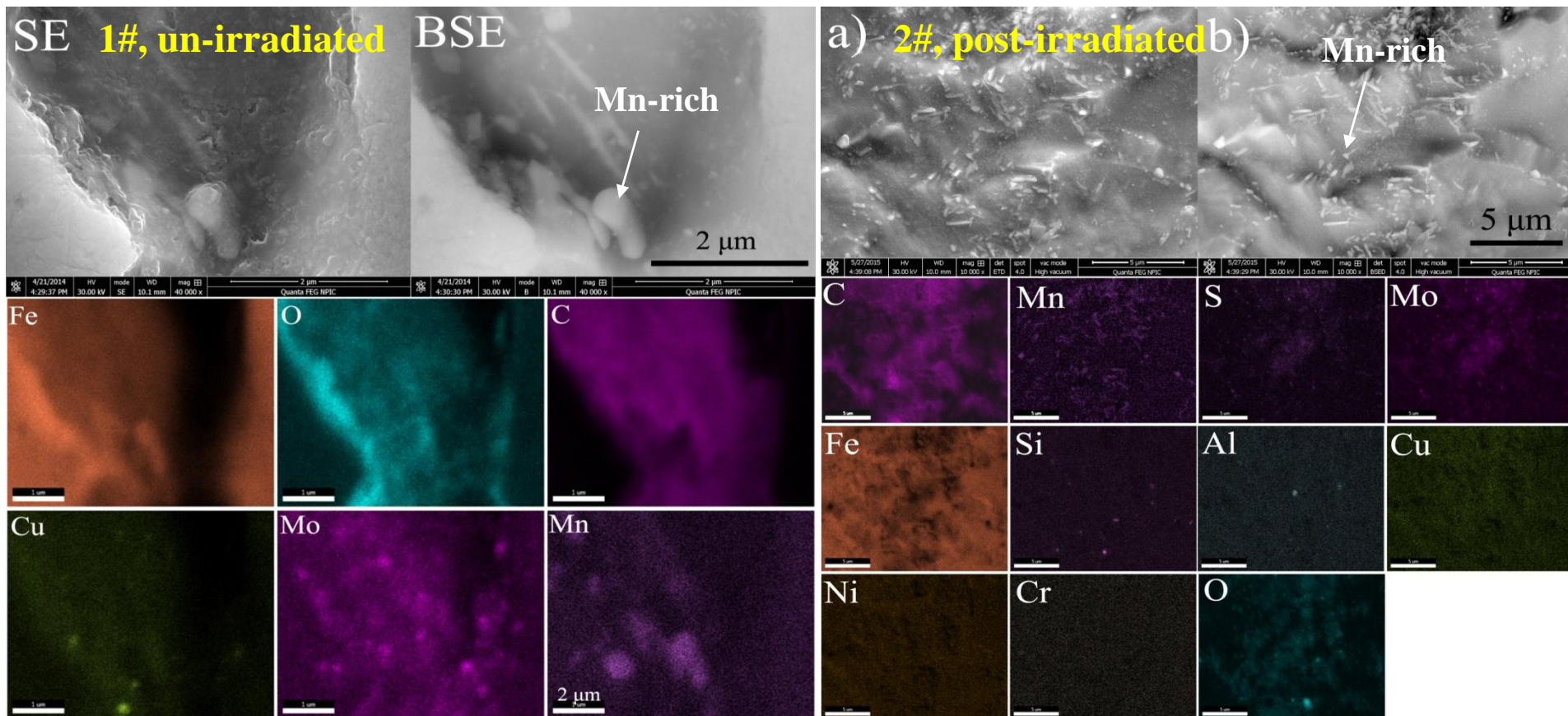
*The evidence of MnS disappeared in post-irradiated samples: the enrichment of Mn and S element among the edge of holes.*

## Reasons:

- ✓ Compare with  $\text{Al}_2\text{O}_3$  and  $\text{MgAl}_2\text{O}_4$ , the melting temperature of MnS is quite lower. MnS is easier to decompose under the hot peak during cascade. In addition, combine with the effect of irradiation enhanced diffusion, S and Mn atoms move to boundaries.
- ✓ In the other hand, Mn atoms transmutation into Fe atoms by nuclear reaction, MnS decompose.



# Results and Discussion



- ✓ Because of low Copper concentration (0.08 wt.%) , very limited Copper clusters could be observed both in un-irradiated and post-irradiated samples
- ✓ Manganese and Molybdenum clusters exist after irradiation





# Conclusions

- ✓ *No obviously change in the bainite structure and grain size of the A508-3 steel could be observed by OM under this irradiate conditions (fluence of neutron is  $2.97 \times 10^{19} \text{ n/cm}^2$ , and irradiation temperature is  $290 \text{ }^\circ\text{C} \pm 15 \text{ }^\circ\text{C}$ ), which could not causing impact energy abnormally.*
- ✓ *The direct reason probably is the differences in fraction volume of the defects(holes) in the matrix, which formed during solidification process.*
- ✓ *The defects could be divided into two types, one is filled with layer-like  $\text{Al}_2\text{O}_3$ ,  $\text{MnS}$ , and  $\text{Al-Mg-O}$  ternary non-metallic inclusions combining together, and the other is holes.*
- ✓ *Boundary between these non-metallic inclusions and matrix is quite loose, which is easily to decrease the impact toughness.*
- ✓ *Except  $\text{MnS}$  phase, the morphology and composition of the  $\text{Al}_2\text{O}_3$  and  $\text{Al-Mg-O}$  ternary non-metallic inclusions in defects were not modified by neutron irradiation significantly under this irradiate conditions.*



# Conclusions



## Next steps:

- ✓ EPMA observation, micro-composition analysis
- ✓ FIB + TEM observation, microstructure analysis
- ✓ Semi in-situ observation



**Thank you for your  
attention!**